

## INVESTIGATION OF THE HEAT CONDUCTIVITY OF MUTUAL SOLUTIONS OF METHYL AND ISOPROPYL ALCOHOLS AT VARIOUS TEMPERATURES AND PRESSURES

Ya. M. Naziev and M. M. Bashirov

UDC 536.223

*The results of an experimental study of the dependence of the heat conductivity of binary solutions of methyl and isopropyl alcohols on the concentration, temperature, and pressure are presented. An empirical equation for calculating this index is proposed.*

The extensive use of aliphatic alcohols in various chemical productions and in many fields of engineering calls for detailed investigations of their thermophysical and thermodynamic properties. Analysis of the literature sources has shown that for a number of aliphatic alcohols the heat conductivity has been studied in a wide range of state parameters [1]. At the present time, however, information about it for mutual solutions of alcohols is actually absent. This induced the authors to study in detail the heat conductivity of binary solutions of methanol with some normal alcohols and isoalcohol.

The heat conductivity of methanol at high pressures was investigated in [2–5] and that of isopropanol — in [2, 6–8]. Comprehensive analysis and comparison of the results of the above publications have shown that to establish the concentration dependence of the heat conductivity of the methanol–isopropanol system, one can successfully use, besides the experimental data obtained by us as reference data, the information for pure methanol from [3, 5] and for pure isopropanol from [6, 7]. This also follows from the fact that the authors of both [3, 6] and the present paper used the regular regime method having in both cases equal systematic errors (1.3%), which were mutually eliminated when the concentration dependence of  $\lambda$  was established.

In the present paper, an experimental study of the heat conductivity of methanol (CH<sub>3</sub>OH)–isopropanol (CH<sub>3</sub>H<sub>7</sub>OH) solutions has been made for mass concentrations of 25, 50, and 75% in the 0.1–50 MPa range of pressures and the 293–500 K range of temperatures.

The investigated alcohols had the following characteristics: methanol — refractive index  $n_D^{20} = 1.3288$ , density  $\rho_4^{20} = 791.15 \text{ kg/m}^3$ , melting temperature  $T_{\text{melt}} = 175.49 \text{ K}$ , boiling temperature  $T_{\text{boil}} = 337.70 \text{ K}$ , critical temperature  $T_{\text{cr}} = 512.64 \text{ K}$ , and critical pressure  $P_{\text{cr}} = 8.096 \text{ MPa}$ ; isopropanol —  $n_D^{20} = 1.3773$ ,  $\rho_4^{20} = 785.2 \text{ kg/m}^3$ ,  $T_{\text{melt}} = 184.68 \text{ K}$ ,  $T_{\text{boil}} = 355.39 \text{ K}$ ,  $T_{\text{cr}} = 508.30 \text{ K}$ , and  $P_{\text{cr}} = 4.762 \text{ MPa}$ .

The experiments were performed by the regular regime method on the set developed by us [9]. Its basic component is a high-pressure tricalorimeter designed to measure the heat conductivity of electrolytes. The design and the principle of operation of the calorimeter are described in [5, 9]. Preliminarily, on the set control measurements of the heat conductivity of model liquids (*n*-heptane and methanol) were made. The results of the experiments were compared with the most reliable literature data. The maximum discrepancy was 2%.

A number of refinements taking into account heat losses in the measuring cells were introduced into the heat-conduction equation [9]. We made no correction for the heat radiation, since alcohols are strongly absorbing liquids. Neither did we make a correction for the heat loss from the ends of the measuring cylinder, since, according to the principle of operation of the new tricalorimeter, it is excluded in the process of heat-conductivity measurement and does not enter into the heat calculation equation.

The absence of convection in the layer of the liquid under investigation is confirmed in experiments by the equal values of the heat conductivity under the same conditions but at different temperature differences between the internal and external cylinders as well as by the fact that the Ra criterion in all cases did not exceed 600.

TABLE 1. Experimental Values of the Heat Conductivity ( $\lambda \cdot 10^4$ , W/(m·K) of Methanol–Isopropanol Solutions

| T, K  | P, MPa |      |      |      |      |      |      |      |
|---|--------|------|------|------|------|------|------|------|
|   | 0.1013 | 1    | 5    | 10   | 20   | 30   | 40   | 50   |
| <i>25 mass % of methanol + 75 mass % of isopropanol</i> |        |      |      |      |      |      |      |      |
| 292.5   | 1475   | 1479 | 1501 | 1527 | 1579 | 1626 | 1671 | 1715 |
| 311.7   | 1434   | 1439 | 1461 | 1487 | 1538 | 1590 | 1636 | 1682 |
| 336.6   | 1386   | 1393 | 1414 | 1440 | 1494 | 1546 | 1594 | 1642 |
| 364.8   |        | 1341 | 1365 | 1395 | 1449 | 1502 | 1550 | 1598 |
| 385.1   |        | 1303 | 1329 | 1363 | 1420 | 1472 | 1521 | 1569 |
| 407.6   |        | 1266 | 1293 | 1331 | 1389 | 1444 | 1495 | 1544 |
| 435.9   |        |      | 1252 | 1293 | 1356 | 1413 | 1465 | 1517 |
| 460.0   |        |      | 1213 | 1261 | 1331 | 1389 | 1446 | 1501 |
| 483.7   |        |      | 1162 | 1221 | 1303 | 1366 | 1426 | 1484 |
| 505.4   |        |      |      | 1174 | 1276 | 1345 | 1410 | 1470 |
| <i>50 mass % of methanol + 50 mass % of isopropanol</i> |        |      |      |      |      |      |      |      |
| 291.9   | 1600   | 1605 | 1632 | 1661 | 1718 | 1769 | 1817 | 1864 |
| 315.5   | 1544   | 1552 | 1575 | 1606 | 1665 | 1717 | 1767 | 1815 |
| 338.1   | 1493   | 1502 | 1527 | 1559 | 1619 | 1673 | 1724 | 1774 |
| 366.2   |        | 1445 | 1473 | 1506 | 1567 | 1622 | 1674 | 1724 |
| 388.4   |        | 1401 | 1431 | 1468 | 1529 | 1587 | 1639 | 1690 |
| 409.8   |        | 1360 | 1394 | 1435 | 1497 | 1559 | 1613 | 1665 |
| 436.2   |        |      | 1350 | 1398 | 1466 | 1527 | 1585 | 1640 |
| 459.7   |        |      | 1309 | 1364 | 1440 | 1503 | 1565 | 1621 |
| 484.3   |        |      | 1249 | 1317 | 1407 | 1477 | 1542 | 1604 |
| 508.6   |        |      |      | 1267 | 1379 | 1456 | 1526 | 1588 |
| <i>75 mass % of methanol + 25 mass % of isopropanol</i> |        |      |      |      |      |      |      |      |
| 292.6   | 1786   | 1791 | 1821 | 1853 | 1912 | 1964 | 2010 | 2055 |
| 313.5   | 1728   | 1736 | 1763 | 1795 | 1856 | 1907 | 1955 | 2004 |
| 334.9   | 1673   | 1681 | 1708 | 1742 | 1805 | 1856 | 1905 | 1955 |
| 360.0   |        | 1623 | 1652 | 1688 | 1749 | 1804 | 1855 | 1904 |
| 387.3   |        | 1561 | 1593 | 1633 | 1693 | 1749 | 1802 | 1853 |
| 408.6   |        | 1519 | 1554 | 1598 | 1660 | 1720 | 1775 | 1826 |
| 439.4   |        |      | 1490 | 1544 | 1615 | 1678 | 1735 | 1789 |
| 460.2   |        |      | 1448 | 1508 | 1587 | 1651 | 1713 | 1768 |
| 482.7   |        |      | 1382 | 1462 | 1550 | 1624 | 1690 | 1748 |
| 507.5   |        |      |      | 1380 | 1506 | 1590 | 1665 | 1727 |

In the experiments, the temperature was measured by a standard PTS-10 resistance thermometer with an error of  $\pm 0.5$  K. The pressure in the experiments was created and measured simultaneously by an MP-600 dead-weight pressure-gauge tester of accuracy class 0.05.

The solutions for the investigations were prepared in a quartz vessel by the gravimetric method on a VLA-200-g-M analytical balance. Chemically pure alcohols were used.

The basic dimensions of the tricalorimeter measuring cell are as follows: the external diameter of the internal measuring cylinder is 12.255 mm, the internal diameter of the external cylinder is 12.931 mm, the value of the annular gap is 0.338 mm, the measuring cylinder length is 140 mm, and the length of the compensation cylinders is 40 mm.

The experiments were performed on isothermic lines with a temperature step of  $\sim 25$  K. The results are presented in Table 1 for rounded values of pressure. The reproducibility of results is  $\sim 0.3\%$ . The top value of temperature in experiments was limited to  $\sim 510$  K for fear of the appearance of thermodiffusion in the solution layer in the vicinity of the pseudocritical point ( $T_{\text{pcr}} = 510.47$  K at  $x_1 = x_2 = 0.5$ ).

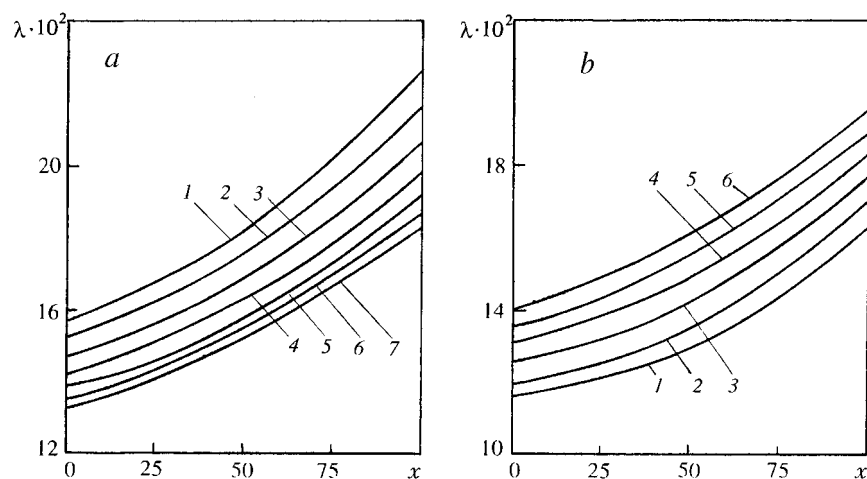


Fig. 1. Heat conductivities of liquid binary methanol-propanol solutions as a function of the methanol concentration: (a) at a pressure of 40 MPa and various temperatures: 1)  $T = 293$ ; 2) 320; 3) 360; 4) 400; 5) 440; 6) 480; 7) 500 K; (b) at a temperature of 460 K and various pressures: 1)  $P = 5$ ; 2) 10; 3) 20; 4) 30; 5) 40; 6) 50 MPa.  $\lambda$ , W/(m·K);  $x$ , mass %.

Figure 1a shows the concentration dependence of the heat conductivity of the methanol-isopropanol solutions at 40 MPa and various temperatures, and Fig. 1b — the same, at 460 K and various pressures. From Table 1 and Fig. 1 it is seen that the heat conductivity of the investigated solutions does not obey the additivity law and deviates from it towards negative values for the region of state parameters (the concentration curves are arranged symmetrically about the straight lines of additivity). In this case, the value of  $\delta\lambda$  depends not only on the concentration of components but also on the temperature and pressure (as the latter increase, it decreases). A similar picture was also observed for other systems of aliphatic alcohols (normal and isoalcohols). Comparison of the concentration dependence of the heat conductivity of the systems methanol-normal alcohols and methanol-isoalcohols shows that it is much stronger for the latter (by about 20%).

Detailed analysis of the experimental data obtained allows us to propose the following empirical equation:

$$\lambda_s = \lambda_1 x_1 + \lambda_2 x_2 + x_1 x_2 (\alpha \Delta T + \beta P - \gamma) 10^{-4}, \quad (1)$$

where  $\Delta T = T - T_0$ ;  $T_0 = (T'_{\text{melt}} + T''_{\text{melt}})/2$ .

For the investigated methanol-isopropanol system we have obtained:  $\alpha = 0.7428$ ,  $\beta = 3.067$ , and  $\gamma = 592.2431$ . The error of equation (1) does not exceed the experimental one.

To generalize the experimental data on the heat conductivity of liquids and gases at high pressures, one may successfully use the Vargaftik dependence [10] relating the excess heat conductivity to the density:

$$\lambda - \lambda_0 = f(\rho). \quad (2)$$

The chief disadvantage of expression (2) is the fact that it includes the density, which itself is thought of as a quantity to be determined and is a function of temperature and pressure. In using formula (2), it is necessary to pre-determine the density, since for many solutions it is not known.

Works [11, 12] give an equation of state of matter well defining experimental density data (with a maximum error of 0.1%):

$$f(\rho) = A_0(T) + B_0(T) P^{0.5} + C_0(T) P. \quad (3)$$

Combining (2) and (3), we can obtain a simple heat-conduction equation in the form

$$(\lambda - \lambda_0)^2 = A(T) + B(T) P^{0.5} + C(T) P. \quad (4)$$

TABLE 2. Values of Coefficients  $a_i$ ,  $b_i$ , and  $c_i$  in Eq. (4)

| $i$ | $a_i$                       | $b_i$                         | $c_i$                      |
|-----|-----------------------------|-------------------------------|----------------------------|
| 0   | 0.03024315344               | $0.86937003 \cdot 10^{-2}$    | $-0.288886 \cdot 10^{-3}$  |
| 1   | $0.438077528 \cdot 10^{-4}$ | $-0.6898569246 \cdot 10^{-4}$ | $0.24853091 \cdot 10^{-5}$ |
| 2   | $-0.3591977 \cdot 10^{-6}$  | $0.17768172 \cdot 10^{-6}$    | $-0.6577933 \cdot 10^{-8}$ |
| 3   | $0.336487445 \cdot 10^{-9}$ | $-0.146694972 \cdot 10^{-9}$  | $0.558719 \cdot 10^{-11}$  |

TABLE 3. Comparison of the Experimental and Calculated (by Eq. (4)) Heat Conductivities for the 50% Methanol + 50% Propanol Solution

| $T, K$ | $\lambda_0, W/(m \cdot K)$ | $P, MPa$ |      |            |      |      |            |      |      |            |
|--------|----------------------------|----------|------|------------|------|------|------------|------|------|------------|
|        |                            | 5        |      |            | 20   |      |            | 40   |      |            |
|        |                            | I        | II   | $\epsilon$ | I    | II   | $\epsilon$ | I    | II   | $\epsilon$ |
| 300    | 159                        | 1610     | 1616 | 0.40       | 1699 | 1703 | 0.24       | 1800 | 1808 | 0.45       |
| 340    | 193                        | 1523     | 1519 | 0.30       | 1615 | 1605 | 0.62       | 1720 | 1710 | 0.60       |
| 380    | 236                        | 1445     | 1447 | 0.14       | 1543 | 1542 | 0.07       | 1651 | 1649 | 0.12       |
| 420    | 283                        | 1375     | 1382 | 0.51       | 1486 | 1499 | 0.90       | 1602 | 1615 | 0.82       |
| 460    | 333                        | 1308     | 1307 | 0.10       | 1439 | 1446 | 0.50       | 1564 | 1566 | 0.13       |
| 480    | 358                        | 1260     | 1261 | 0.10       | 1413 | 1413 | 0          | 1546 | 1543 | 0.20       |
| 500    | 384                        |          |      |            | 1384 | 1381 | 0.22       | 1529 | 1534 | 0.33       |

Note: I) experiment; II) calculation;  $\epsilon = (\lambda_{calc} - \lambda_{exp}) \cdot 100 / \lambda_{exp}, \%$ .

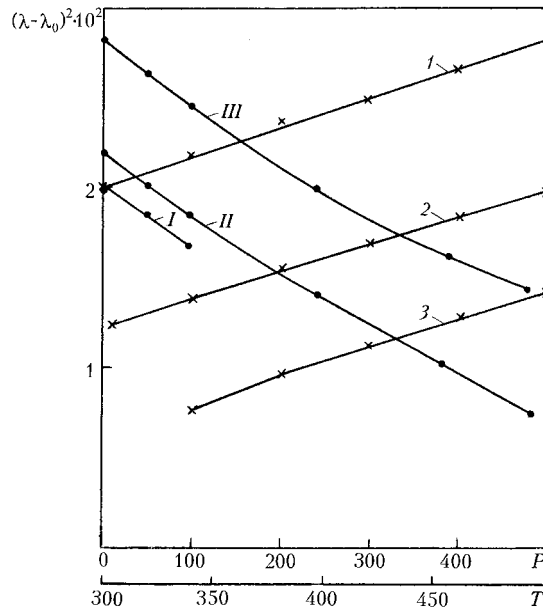


Fig. 2. Excess heat conductivity of the 50% methanol + 50% propanol solution as a function of pressure and temperature: 1) 300; 2) 400; 3) 500 K; I) 1 bar; II) 100; III) 500 bars.  $(\lambda - \lambda_0)^2, (W/(m \cdot K))^2; P, bar; T, K$ .

For approximate calculations, we have

$$(\lambda - \lambda_0)^2 = A'(T) + C'(T)P. \quad (5)$$

In Eqs. (4) and (5),  $P$  is determined in bars.

The constants  $A(T)$ ,  $B(T)$ ,  $C(T)$ ,  $A'(T)$ , and  $C'(T)$  are found from the experimental data. It should be noted that the value of  $\lambda_0$  for solutions can be found from the additivity law, since for the gas phase the deviation of the heat conductivity from the additivity line is insignificant. Moreover, always  $\lambda_0 < \lambda$ . Thus, Eq. (4) can be used successfully for solutions.

The use of dependences (4) and (5) for methanol and isopropanol and their solutions has shown that both equations are convenient for practical use, but (4) is more exact and convenient, although it contains more coefficients.

The values of the coefficients of Eq. (4) were found on a computer by the least-squares method and are given in Table 2:

$$A = \sum_{i=0}^3 a_i T^i, \quad B = \sum_{i=0}^3 b_i T^i, \quad C = \sum_{i=0}^3 c_i T^i. \quad (6)$$

We have used Eq. (4) to generalize the data on  $\lambda$  of a 50% methanol + 50% isopropanol solution. Table 3 compares smoothed experimental and calculated values of the heat conductivities of the solution. The results of the comparison are quite satisfactory. The maximum discrepancy is 0.9% at  $T = 420$  K and  $P = 20$  MPa.

The dependence of the excess heat conductivity of the solution of 50% methanol + 50% isopropanol is shown in Fig. 2, from which it is seen that the dependence  $(\Delta\lambda)^2 = f(P)$  is almost rectilinear.

## NOTATION

$n_D^{20}$ , refractive index;  $\lambda$ , heat conductivity of liquid at various  $P$  and  $T$ , W/(m·K);  $\lambda_0$ , heat conductivity of gas at atmospheric pressure and at different  $T$ ;  $\lambda_s$ , heat conductivity of solution;  $\lambda_1$  and  $\lambda_2$ , heat conductivities of the first and second components of the solution;  $\delta\lambda$ , value of deviation of the experimental heat conductivity from the additive one;  $\Delta\lambda = (\lambda - \lambda_0)$ , excess heat conductivity (difference of the heat conductivities of liquid and gas);  $x_1$  and  $x_2$ , concentrations of the first and second components, in fractions;  $P$ , pressure, MPa;  $T$ , temperature, K;  $T_0$ , base temperature;  $T'_{\text{melt}}$  and  $T''_{\text{melt}}$ , melting temperatures of the first and second components; Ra, Rayleigh criterion;  $\varepsilon$ , error of the calculated equation (4) compared to the experimental data;  $\rho$ , liquid density at various  $P$  and  $T$ , kg/m<sup>3</sup>;  $\alpha$ ,  $\beta$ ,  $\gamma$ , constants for the given system;  $A_0(T)$ ,  $B_0(T)$ ,  $C_0(T)$ , constants for determining the density;  $A(T)$ ,  $B(T)$ ,  $C(T)$ ,  $A'(T)$ ,  $C'(T)$ , constants for determining the excess heat conductivity. Subscripts:  $a$ ,  $b$ ,  $c$ , coefficients of polynomials; melt, melting; s, solution; pcr, pseudocritical; exp, experimental; boil, boiling; cr, critical; calc, calculated;  $i$ , number of polynomial members.

## REFERENCES

1. Ya. M. Naziev, A. N. Shakhverdiev, N. S. Aliev, and M. M. Bashirov, *Thermal Properties of Monobasic Alcohols (Heat Conductivity). Reviews on the Thermophysical Properties of Substances* [in Russian], Moscow (1992).
2. P. Bridgman, *The Physics of High Pressures* [Russian translation], Moscow–Leningrad (1935).
3. I. F. Golubev and T. N. Vasil'kovskaya, *Teploenergetika*, No. 5, 77–81 (1969).
4. I. Kh. Mukhamedziyanov, *Experimental Study of Heat Conductivity of Liquid Organic Compounds at Pressures up to 2500 bars*, Author's Abstract of Candidate Dissertation (in Engineering), Kazan' (1972).
5. M. M. Bashirov and Ya. M. Naziev, *Probl. Energet.*, No. 4, 133–139 (2001).
6. T. N. Vasil'kovskaya and I. F. Golubev, in: *Chemistry and Technology of Nitrogenous Fertilizers and Products of Organic Synthesis* [in Russian], Issue 23, Moscow (1969), pp. 121–135.
7. T. N. Vasil'kovskaya and I. F. Golubev, *Teploenergetika*, No. 6, 84–86 (1969).
8. H. Forsman, P. Anderson, and F. Bacstrom, *Physica*, **114B**, No. 3, 287–294 (1982).
9. Ya. M. Naziev and M. M. Bashirov, *Izv. Ross. Akad. Nauk, Energetika*, No. 3, 157–162 (2002).
10. N. B. Vargaftik, *Heat Conductivity of Compressed Liquids and Gases*, Author's Abstract of Doctoral Dissertation (in Engineering), Moscow (1952).
11. Ya. M. Naziev and V. G. Gasanov, *Zh. Prikl. Khim.*, **68**, Issue 2, 210–213 (1995).
12. S. S. Tsimmerman and V. M. Miniovich, *Zh. Fiz. Khim.*, **51**, No. 1, 208–209 (1977).